DAY 1 Work Problems

- Sediment Trap
- Sediment Basin

SEDIMENT TRAP CALCULATIONS ESCH III-70-76
Total drainage area <3 acres

1. **Given a total drainage area of 2.5 acres, what is the total volume (V) of sediment trap required?**

$$V = A \times 134$$

V (Total Volume, cubic yards) = A (Total Drainage Area, acres) x 134(cubic yards/acres)

V = ( )acres x 134 (cubic yards/acres) = ( ) cubic yards

2. **If the drainage are is 1.5 acres, what volume (V) is required for the permanent pool for wet storage?**

$$V = A \times 67$$

V (Perm. Pool Vol., cubic yards) = A (Total Drainage Area, acres) x 67(cubic yards/acre)

V = ( )acres x 67(cubic yards/acres) = ( )cubic yards

3. **For a total drainage are of 2.8 acres, how much volume (V) is required for the temporary pool or drawdown volume for dry storage?**

$$V = A \times 67$$

V (Temp. Pool Vol., cubic yards) = A (Total Drainage Area, acres) x 67(cubic yards/acres)

V = ( )acres x 67(cubic yards/acres) = ( )cubic yards

4. **If the sediment trap receives drainage from 0.75 acres of disturbed area onsite and receives runoff from 1.5 acres of undisturbed area offsite, at what volume (V) should sediment be removed?**

$$V = A \times \frac{67}{2} = A \times 33.5$$

V (Sediment Vol., cubic yards) = A (Total Drainage Area, acres) x 33.5(cubic yards/acres)

V = ( )acres x 33.5(cubic yards/acres) = ( )cubic yards

5. **What is the minimum length (L) of outlet required for a sediment trap with a drainage area of 1.9 acres?**

$$L = A \times 6$$

L (Outlet Length, feet) = A (Total Drainage Area, acres) x 6(feet/acre)

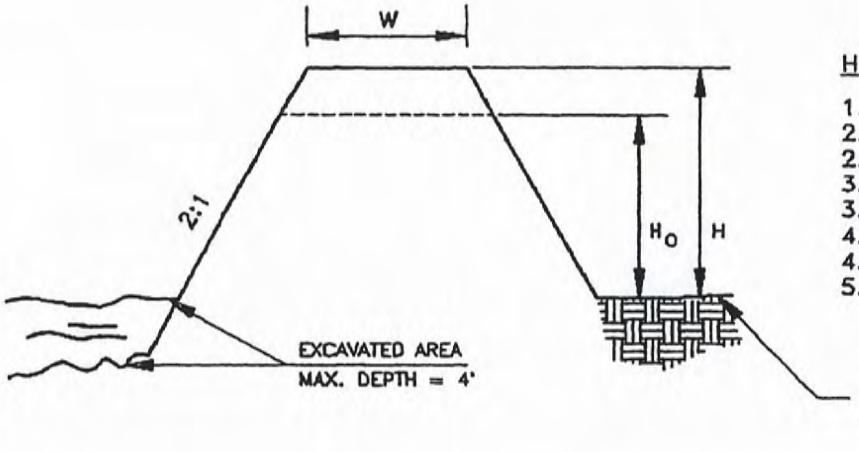
L = ( )acres x 6(feet/acres) = ( )feet

6. **If a sediment trap has a 4.5 feet high embankment, what is the minimum top width required on the embankment?**

From ESCH III-74, Plate 3.13-1

Embankment Height, H = ( )feet Top Width, W = ( )feet

MINIMUM TOP WIDTH (W) REQUIRED FOR SEDIMENT TRAP EMBANKMENTS ACCORDING TO HEIGHT OF EMBANKMENT (FEET)



H	H_O	W
1.5	0.5	2.0
2.0	1.0	2.0
2.5	1.5	2.5
3.0	2.0	2.5
3.5	2.5	3.0
4.0	3.0	3.0
4.5	3.5	4.0
5.0	4.0	4.5

Source: Va. DSWC

Plate 3.13-1

SEDIMENT BASIN CALCULATIONS ESCH III-77-115

Total Drainage Area between 3 and 100 acres

1. **For a total drainage area of 25 acres, what volume (V) sediment basin is required?**

$$V = A \times 134$$

V (Total Volume, cubic yards) = A (Total Drainage Area, acres) x 134(cubic yards/acre)

V = ( ) acres x 134(cubic yards/acre) = ( ) cubic yards

2. **If the total drainage area is 18 acres, what is the volume (V) of the permanent pool or wet storage?**

$$V = A \times 67$$

V (Perm Pool Vol., cubic yards) = A (Total Drainage Area, acres) x 67(cubic yards/acres)

V = ( ) acres x 67(cubic yards/acres) = ( ) cubic yards

3. **Given 5 acres of disturbed area onsite and 10 acres undisturbed above the site but draining to the sediment basin, what is the required volume (V) of the temporary pool or drawdown volume?**

$$V = A \times 67$$

V (Temp. Pool Vol., cubic yards/acres) = A (Total Drainage Area, acres) x 67(cubic yards/acres)

V = ( ) acres x 67(cubic yards/acre) = ( ) cubic yards

4. **Given that the sediment cleanout level shall be no higher than one foot below the dewatering device, determine the maximum volume (V) of sediment that will require removal from the permanent pool of a sediment basin serving 27 acres?**

$$V = A \times \frac{67}{2} = A \times 33.5$$

V (Sediment Vol., (cubic yards) = A (Total Drainage Area, acres) x 33.5(cubic yards/acres)

V = ( ) acres x 33.5(cubic yards/acres) = ( ) cubic yards

5. If a plan shows a sediment basin with a flow length of 125 feet, what is the maximum effective width required such that no baffles are required?

$$\frac{L}{W_e} = x$$

$$x \geq 2 \ldots \textit{no baffles required}$$
$$x < 2 \ldots \textit{baffles required}$$

L (Flow length, feet) / W_e (Effective Width, feet) $\geq$ 2 (no baffles; < 2 (baffles required)

$$\frac{L}{W_e} = 2$$

or

$$W_e = \frac{L}{2}$$

W_e(feet) = L(feet) / 2 = ( )feet / 2 = ( )

6. **What is the minimum top width of a sediment basin embankment with a 15 feet height?**

From ESCH III-80:

Embankment Height	**Minimum Top Width**
< 10 feet	6 feet
10-14 feet	8 feet
15 feet (max)	10 feet

H (Embankment Height, feet) = ( ) feet

T (Minimum Top Width, feet) = ( ) feet

7. What is the diameter in inches of the dewatering orifice for a sediment basin draining 15 acres?

A. Determine temporary pool or dry storage volume.

$$V = A \times 67$$

V (Temp. Pool Vol., cubic yards) = A (Drainage Area, acres) x 67 (cubic yards/acres)

V = ( ) acres x 67(cubic yards/acres) = ( ) cubic yards

B. Convert temporary pool volume from cubic yards to cubic feet.

cubic feet = cubic yards x 27

V (Temp. Pool Vol., cubic feet) = V (Temp. Pool Vol., cubic yards) x 27

V (cubic feet) = ( ) cubic yards x 27 = ( ) cubic feet

C. What is the flow rate through the orifice for a 6 hour drawdown?

$$Q = \frac{V}{t}$$

where

t = drawdown time in seconds (6 x 60 x 60)

or

$$Q = \frac{V}{21{,}600}$$

Q (Flow Rate, cubic feet/second) = V (Temp. Pool Volume, cubic feet) / 21,600 (seconds)

Q (cubic feet/second) = ( ) cubic feet / 21,600 (seconds) = ( ) cfs

D. If the maximum possible head is 2 feet, what is the average driving head?

$$h = \frac{H}{2}$$

h (Average Driving Head, feet) = H (Maximum Possible Heat, feet) / 2

H (feet) = ( ) feet / 2 = ( ) feet

E. Given the Flow Rate, Q, from C and the Average Driving Head, h, from D, what is the orifice area?

$$A = \frac{Q}{\left(\sqrt{64.32xh}\right) \times 0.6}$$

or

$$A = \frac{Q}{(64.32 \times h)^{\frac{1}{2}} \times 0.6}$$

A (Orifice Area, square feet) = Q (Flow Rate, cfs) / {[64.32 x h (average driving, feet)]$^{1/2}$ x (0.6)}

A = ( ) cfs / {[64.32 x ( ) feet]$^{1/2}$ x (0.6)} = ( ) square feet

F. What is the orifice diameter?

$$d = 2 \times \sqrt{\left(\frac{A}{3.14}\right)}$$

or

$$d = 2 \times \left(\frac{A}{3.14}\right)^{\frac{1}{2}}$$

d (Orifice diameter, feet) = 2 x [A (Orifice area, square feet) / 3.14]$^{1/2}$

d (feet) = 2 x [( ) square feet / 3.14]$^{1/2}$ = ( ) feet

G. What is the orifice diameter in inches?

$$D = d \times 12$$

D (Orifice diameter, inches) = d (Orifice diameter, feet) x 12(inches/foot)

H. For this size orifice, what is the diameter of the perforated drainage tubing?

$$D_t = D + 2$$

D_t (Diameter of tubing, inches) = D (Orifice diameter, inches) + 2(inches)

D_t (inches) = ( ) inches + 2(inches) = ( ) inches

8. **What diameter riser is required for a principle spillway with a peak flow of 25cfs and 1.0 feet head?**

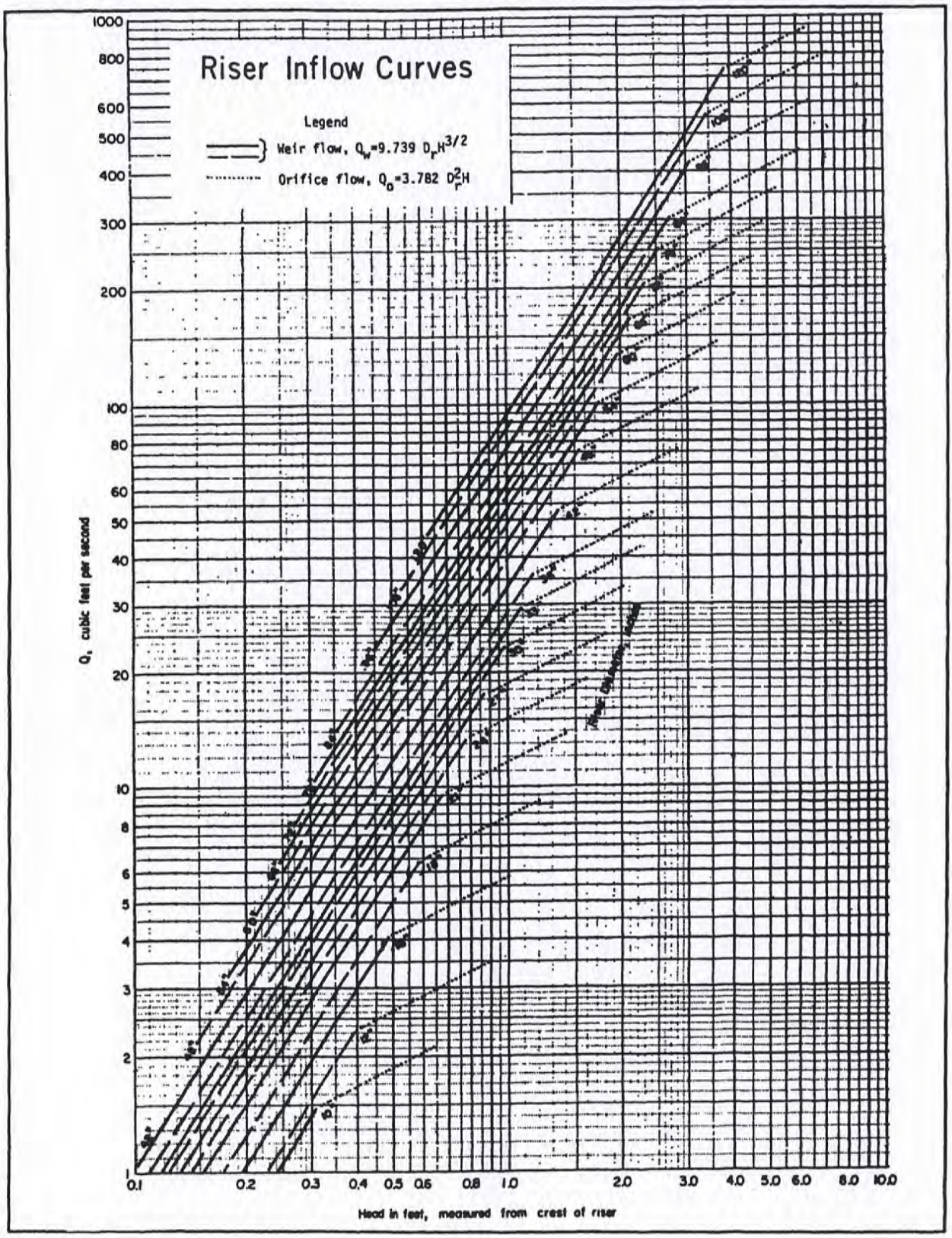
From ESCH III-97, Plate 3.14-8:

On horizontal axis, select head, h (feet), and read up.

On vertical axis, select peak flow, Q (cfs), and read across.

At intersection of two lines, read riser diameter.

Riser Diameter = ( )inches.



Source: USDA-SCS

Plate 3.14-8

9. **Given an 80 feet long, corrugated metal pipe, what is the diameter of the barrel required for a peak flow, Q = 25(cfs) and head, H = 10(feet) on pipe outside embankment.**

From ESCH III-98 (corrugated metal pipe):

On the left vertical column, select the head, H (feet) = ( )feet

Read across the table, select the pipe peak flow, Q_{70} (cfs) = ( )cfs

Read up the table to determine the pipe diameter, D (inches) = ( )inches

If pipe length is other than 70 feet long: L (feet) = ( )feet

Read from bottom of chart for the pipe length, the Conversion Factor, CF = ( )

The pipe capacity for this length pipe is determined:

$$Q_L = CF \times Q_{70}$$

Q_L (Pipe Capacity, cfs) = CF (Conversion Factor) x Q_{70} (Pipe Peak Flow, cfs)

Q_L = ( ) x ( ) cfs = ( ) cfs

If pipe capacity flow rate, Q_L (cfs) is less than the required peak flow rate, Q (cfs), select the next larger pipe size and repeat above calculation.

Pipe Diameter, D = ( ) inches

TABLE 3.14-A
PIPE FLOW CHART, n = 0.025

FOR CORRUGATED METAL PIPE INLET $K_m = K_e + K_b = 1.0$ AND 70 FEET OF CORRUGATED METAL PIPE CONDUIT (full flow assumed)
Note correction factors for pipe lengths other than 70 feet
diameter of pipe in inches

H, in feet	6"	8"	10"	12"	15"	18"	21"	24"	30"	36"	42"	48"	54"	60"	66"	72"	78"	84"	90"	96"	102"
1	0.33	0.70	1.25	1.98	3.48	5.47	7.99	11.0	18.8	28.8	41.1	55.7	72.6	91.8	113	137	163	191	222	255	290
2	0.47	0.99	1.76	2.80	4.92	7.74	11.3	15.6	26.6	40.8	58.2	78.8	103	130	160	194	231	271	314	360	410
3	0.58	1.22	2.16	3.43	6.02	9.48	13.8	19.1	32.6	49.9	71.2	96.5	126	159	196	237	282	331	384	441	502
4	0.67	1.40	2.49	3.97	6.96	10.9	16.0	22.1	37.6	57.7	82.3	111	145	184	226	274	326	383	444	510	580
5	0.74	1.57	2.79	4.43	7.78	12.2	17.9	24.7	42.1	64.5	92.0	125	162	205	253	306	365	428	496	570	648
6	0.82	1.72	3.05	4.86	8.52	13.4	19.6	27.0	46.1	70.6	101	136	178	225	277	336	399	469	544	624	710
7	0.88	1.86	3.30	5.25	9.20	14.5	21.1	29.2	49.8	76.3	109	147	192	243	300	362	431	506	587	674	767
8	0.94	1.99	3.53	5.61	9.84	15.5	22.6	31.2	53.2	81.5	116	158	205	260	320	388	461	541	628	721	820
9	1.00	2.11	3.74	5.95	10.4	16.4	24.0	33.1	56.4	86.5	123	167	218	275	340	411	489	574	666	764	870
10	1.05	2.22	3.94	6.27	11.0	17.3	25.3	34.9	59.5	91.2	130	176	230	290	358	433	516	605	702	806	917
11	1.10	2.33	4.13	6.58	11.5	18.2	26.5	36.6	62.4	95.6	136	185	241	304	376	454	541	635	736	845	962
12	1.15	2.43	4.32	6.87	12.1	19.0	27.7	38.2	65.2	99.9	142	193	252	318	392	475	565	663	769	883	1004
13	1.20	2.53	4.49	7.15	12.6	19.7	28.8	39.8	67.8	104	148	201	262	331	408	494	588	690	800	919	1045
14	1.25	2.63	4.66	7.42	13.0	20.5	29.9	41.3	70.4	108	154	208	272	343	424	513	610	716	830	953	1085
15	1.29	2.72	4.83	7.68	13.5	21.2	30.9	42.8	72.8	112	159	216	281	355	439	531	631	741	860	987	1123
16	1.33	2.81	4.99	7.93	13.9	21.9	32.0	44.2	75.2	115	165	223	290	367	453	548	652	765	888	1019	1160
17	1.37	2.90	5.14	8.18	14.3	22.6	32.9	45.5	77.5	119	170	230	229	378	467	565	672	789	915	1051	1195
18	1.41	2.98	5.29	8.41	14.8	23.2	33.9	46.8	79.8	120	174	236	308	389	480	581	692	812	942	1081	1230
19	1.45	3.06	5.43	8.64	15.2	23.9	34.8	48.1	82.0	126	179	243	316	400	494	597	711	834	967	1111	1264
20	1.49	3.14	5.57	8.87	15.6	24.5	35.7	49.4	84.1	129	184	249	325	410	506	613	729	856	993	1139	1297
21	1.53	3.22	5.71	9.09	15.9	25.1	36.6	50.6	86.2	132	188	255	333	421	519	628	747	877	1017	1168	1329
22	1.56	3.29	5.85	9.30	16.3	25.7	37.5	51.8	88.2	135	193	261	341	430	531	643	765	898	1041	1195	1360
23	1.60	3.37	5.98	9.51	16.7	26.2	38.3	53.0	90.2	138	197	267	348	440	543	657	782	918	1064	1222	1390
24	1.63	3.44	6.11	9.72	17.0	26.8	39.1	54.1	92.1	141	201	273	356	450	555	671	799	937	1087	1248	1420
25	1.66	3.51	6.23	9.92	17.4	27.4	39.9	55.2	94.0	144	206	279	363	459	566	685	815	957	1110	1274	1450
26	1.70	3.58	6.36	10.1	17.7	27.9	40.7	56.3	95.9	147	210	284	370	468	577	699	831	976	1132	1299	1478
27	1.73	3.65	6.48	10.3	18.1	28.4	41.5	57.4	97.7	150	214	290	377	477	588	712	847	994	1153	1324	1507
28	1.76	3.72	6.60	10.5	18.4	29.0	42.3	58.4	99.5	153	218	295	384	486	599	725	863	1013	1174	1348	1534
29	1.79	3.78	6.71	10.7	18.7	29.5	43.0	59.5	101	155	221	300	391	494	610	738	878	1030	1195	1372	1561
30	1.82	3.85	6.83	10.9	19.1	30.0	43.7	60.5	103	158	225	305	398	503	620	750	893	1048	1216	1396	1588
L, in feet	Correction Factors For Other Pipe Lengths																				
20	1.69	1.63	1.58	1.53	1.47	1.42	1.37	1.34	1.28	1.24	1.20	1.18	1.16	1.14	1.13	1.11	1.10	1.10	1.09	1.08	1.08
30	1.44	1.41	1.39	1.36	1.32	1.29	1.27	1.24	1.21	1.18	1.15	1.13	1.12	1.11	1.10	1.09	1.08	1.07	1.07	1.06	1.06
40	1.28	1.27	1.25	1.23	1.21	1.20	1.18	1.17	1.14	1.12	1.11	1.10	1.09	1.08	1.07	1.06	1.06	1.05	1.05	1.05	1.04
50	1.16	1.16	1.15	1.14	1.13	1.12	1.11	1.10	1.09	1.08	1.07	1.06	1.06	1.05	1.05	1.04	1.04	1.04	1.03	1.03	1.03
60	1.07	1.07	1.07	1.06	1.06	1.05	1.05	1.05	1.04	1.04	1.03	1.03	1.03	1.02	1.02	1.02	1.02	1.02	1.02	1.02	1.01
70	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
80	.94	.94	.95	.95	.95	.95	.96	.96	.96	.97	.97	.97	.98	.98	.98	.98	.98	.98	.99	.99	.99
90	.89	.89	.90	.90	.91	.91	.92	.92	.93	.94	.94	.95	.95	.96	.96	.96	.97	.97	.97	.97	.94
100	.85	.85	.86	.86	.87	.88	.89	.89	.90	.91	.92	.93	.93	.94	.94	.95	.95	.95	.96	.96	.94
120	.78	.79	.79	.90	.81	.82	.83	.83	.85	.86	.87	.89	.89	.90	.91	.89	.92	.93	.93	.94	.92
140	.72	.73	.74	.75	.76	.77	.78	.79	.81	.82	.84	.85	.86	.87	.88	.86	.89	.90	.91	.91	.90
160	.68	.69	.69	.70	.71	.73	.74	.75	.77	.79	.80	.82	.83	.84	.85	.92	.87	.88	.89	.89	

Source: USDA-SCS

10. **For a 50 cfs peak flow rate, what diameter of 100 feet long reinforced concrete pipe is required given a head of 11 feet on the pipe outside embankment?**

From ESCH III-99 (reinforced concrete pipe):

On the left vertical column, select the head, H(feet) = ( )feet

Read across the table, select the pipe peak flow, Q_{70}(cfs) = ( )cfs

Read up the table to determine the pipe diameter, D(inches) = ( )inches

If pipe length is other than 70 feet long: L(feet) = ( )feet

Read from bottom of chart for the pipe length, the Conversion Factor, CF = ( )

The pipe capacity for this length pipe is determined:

$$Q_L = CF \times Q_{70}$$

Q_L (Pipe Capacity, cfs) = CF (Conversion Factor) x Q_{70} (Pipe Peak Flow, cfs)

Q_L = ( ) x ( ) cfs = ( ) cfs

If pipe capacity flow rate, Q_L(cfs) is less than the required peak flow rate, Q(cfs), select the next larger pipe size and repeat above calculation.

Pipe Diameter, D = ( ) inches

TABLE 3.14-B
PIPE FLOW CHART, n = 0.013

FOR REINFORCED CONCRETE PIPE INLET $K_m = K_e + K_b = 0.65$ AND 70 FEET OF REINFORCED CONCRETE PIPE CONDUIT (full flow assumed)

Note correction factors for pipe lengths other than 70 feet

diameter of pipe in inches

H, in feet	12"	15"	18"	21"	24"	30"	36"	42"	48"	54"	60"	66"	72"	78"	84"	90"	96"	102"
1	3.22	5.44	8.29	11.8	15.9	26.0	38.6	53.8	71.4	91.5	114	139	167	197	229	264	302	342
2	4.55	7.69	11.7	16.7	22.5	36.8	54.6	76.0	101	129	161	197	236	278	324	374	427	483
3	5.57	9.42	14.4	20.4	27.5	45.0	66.9	93.1	124	159	198	241	289	341	397	458	523	592
4	6.43	10.9	16.6	23.5	31.8	52.0	77.3	108	143	183	228	278	334	394	459	529	604	683
5	7.19	12.2	18.5	26.3	35.5	58.1	86.4	120	160	205	255	311	373	440	513	591	675	764
6	7.88	13.3	20.3	28.8	38.9	63.7	94.6	132	175	224	280	341	409	482	562	647	739	837
7	8.51	14.4	21.9	31.1	42.0	68.8	102	142	189	242	302	368	441	521	607	699	798	904
8	9.10	15.4	23.5	33.3	44.9	73.5	109	152	202	259	323	394	472	557	685	748	854	966
9	9.65	16.3	24.9	35.3	47.7	78.0	116	161	214	275	342	418	500	590	688	793	905	1025
10	10.2	17.2	26.2	37.2	50.2	82.2	122	170	226	289	361	440	527	622	725	836	954	1080
11	10.7	18.0	27.5	39.0	52.7	86.2	128	178	237	304	379	462	553	653	761	877	1001	1133
12	11.1	18.9	28.7	40.8	55.0	90.1	134	186	247	317	395	482	578	682	794	916	1045	1184
13	11.6	19.6	29.9	42.4	57.3	93.7	139	194	257	330	411	502	601	710	827	953	1088	1232
14	12.0	20.4	31.0	44.1	59.4	97.3	145	201	267	342	427	521	624	736	858	989	1129	1278
15	12.5	21.1	32.1	45.6	61.5	101	150	208	277	354	442	539	646	762	888	1024	1169	1323
16	12.9	21.8	33.2	47.1	63.5	104	155	215	286	366	457	557	667	787	917	1057	1207	1367
17	13.3	22.4	34.2	48.5	65.5	107	159	222	294	377	471	574	688	812	946	1090	1244	1409
18	13.7	23.1	35.2	49.9	67.4	110	164	228	303	388	484	591	708	835	973	1121	1280	1450
19	14.0	23.7	36.1	51.3	69.2	113	168	234	311	399	497	607	727	858	1000	1152	1315	1489
20	14.4	24.3	37.1	52.6	71.0	116	173	240	319	409	510	623	746	880	1026	1182	1350	1528
21	14.7	24.9	38.0	53.9	72.8	119	177	246	327	419	523	638	764	902	1051	1211	1383	1566
22	15.1	25.5	38.9	55.2	74.5	122	181	252	335	429	535	653	782	923	1076	1240	1415	1603
23	15.4	26.1	39.8	56.5	76.2	125	186	258	342	439	547	668	800	944	1100	1268	1447	1639
24	15.8	26.7	40.6	57.7	77.8	127	189	263	350	448	559	682	817	964	1123	1295	1478	1674
25	16.1	27.2	41.5	58.9	79.4	130	193	269	357	458	571	696	834	984	1147	1322	1509	1708
26	16.4	27.7	42.3	60.0	81.0	133	197	274	364	467	582	710	850	1004	1169	1348	1539	1742
27	16.7	28.3	43.1	61.2	82.5	135	201	279	371	476	593	723	867	1023	1192	1373	1568	1775
28	17.0	28.8	43.9	62.3	84.1	138	204	285	378	484	604	737	883	1041	1214	1399	1597	1808
29	17.3	29.3	44.7	63.4	85.5	140	208	290	384	493	615	750	898	1060	1235	1423	1625	1840
30	17.6	29.8	45.4	64.5	87.0	142	212	294	391	501	625	763	913	1078	1256	1448	1653	1871
L, in feet	Correction Factors For Other Pipe Lengths																	
20	1.30	1.24	1.21	1.18	1.15	1.12	1.10	1.08	1.07	1.06	1.05	1.05	1.04	1.04	1.03	1.03	1.03	1.03
30	1.22	1.18	1.15	1.13	1.12	1.09	1.08	1.06	1.05	1.05	1.04	1.04	1.03	1.03	1.03	1.02	1.02	1.02
40	1.15	1.13	1.11	1.10	1.08	1.07	1.05	1.05	1.04	1.03	1.03	1.03	1.02	1.02	1.02	1.02	1.02	1.02
50	1.09	1.08	1.07	1.06	1.05	1.04	1.04	1.03	1.03	1.02	1.02	1.02	1.02	1.01	1.01	1.01	1.01	1.01
60	1.04	1.04	1.03	1.03	1.03	1.02	1.02	1.02	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01
70	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
80	.96	.97	.97	.97	.98	.98	.98	.99	.99	.99	.99	.99	.99	.99	.99	.99	.99	.99
90	.93	.94	.94	.95	.95	.96	.97	.97	.98	.98	.98	.98	.98	.99	.99	.99	.99	.99
100	.90	.91	.92	.93	.93	.95	.95	.96	.97	.97	.97	.98	.98	.98	.98	.98	.98	.99
120	.84	.86	.87	.89	.90	.91	.93	.94	.94	.95	.96	.96	.96	.97	.97	.97	.97	.98
140	.80	.82	.83	.85	.86	.88	.90	.91	.92	.93	.94	.94	.95	.95	.96	.96	.96	.97
160	.76	.78	.80	.82	.83	.86	.88	.89	.90	.91	.92	.93	.94	.94	.95	.95	.95	.96

Source: USDA-SCS

11. **Given a 21 inch corrugated metal pipe riser, what is the diameter, thickness, and height of the trash rack and anti-vortex device?**

From ESCH III-104, Table 3.14-D:

Read Riser Diameter, D = ( ) inches

Read horizontally across table to determine:

Cylinder Diameter = ( ) inches

Cylinder Thickness = ( ) gage

Height = ( ) inches

TABLE 3.14-D

CONCENTRIC TRASH RACK AND ANTI-VORTEX DEVICE DESIGN TABLE

Riser Diam., in.	Cylinder		Height, inches	Minimum Size Support Bar	Minimum Top	
	Diameter, inches	Thickness, gage			Thickness	Stiffener
12	18	16	6	#6 Rebar or 1½ x 1½ x 3/16 angle	16 ga. (F&C)	-
15	21	16	7	" "	" "	-
18	27	16	8	" "	" "	-
21	30	16	11	" "	16 ga.(C), 14 ga.(F)	-
24	36	16	13	" "	" "	-
27	42	16	15	" "	" "	-
36	54	14	17	#8 Rebar	14 ga.(C), 12 ga.(F)	-
42	60	16	19	" "	" "	-
48	72	16	21	1¼" pipe or 1¼ x 1¼ x ¼ angle	14 ga.(C), 10 ga.(F)	-
54	78	16	25	" "	" "	-
60	90	14	29	1½" pipe or 1½ x 1½ x ¼ angle	12 ga.(C), 8 ga.(F)	-
66	96	14	33	2" pipe or 2 x 2 x 3/16 angle	12 ga.(C), 8 ga.(F) w/stiffener	2 x 2 x ¼ angle
72	102	14	36	" "	" "	2½ x 2½ x ¼ angle
78	114	14	39	2½" pipe or 2 x 2 x ¼ angle	" "	" "
84	120	12	42	2½" pipe or 2½ x 2½ x ¼ angle	" "	2½ x 2½ x 5/16 angle

Note$_1$: The criterion for sizing the cylinder is that the area between the inside of the cylinder and the outside of the riser is equal to or greater than the area inside the riser. Therefore, the above table is invalid for use with concrete pipe risers.
Note$_2$: Corrugation for 12"-36" pipe measures 2⅔" x ½"; for 42" -84" the corrugation measures 5" x 1" or 8" x 1".
Note$_3$: C = corrugated; F = flat.

Source: Adapted from USDA-SCS and Carl M. Henshaw Drainage Products Information.

12. For a sediment basin embankment less than 10 feet high, what size concrete base is required for a riser of 24 inches diameter to prevent floating?

From ESCH III-110, Plate 3.14-14:

$$CBD = 2 \times D$$

CBD (Concrete Base Dimension, inches) = 2 x D (Diameter of Riser, inches)

CBD = 2 x ( ) inches = ( ) inches

13. What size steel plate is required to anchor the principal spillway of a sediment basin with an embankment less than 10 feet high and a riser of 36 inches diameter?

From ESCH III-110, Plate 3.14-14:

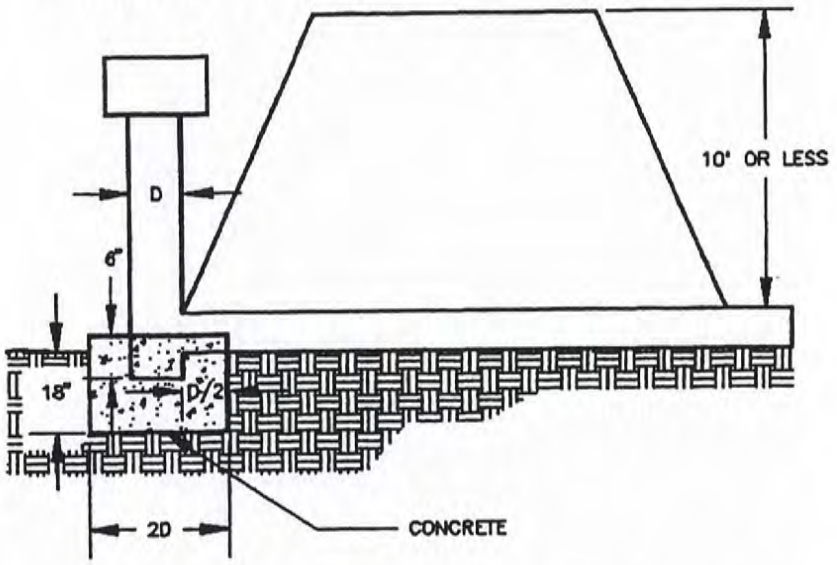
$$SBD = 2 \times D$$

SBD (Steel Base Dimension, inches) = 2 x D (Diameter of Riser, inches)

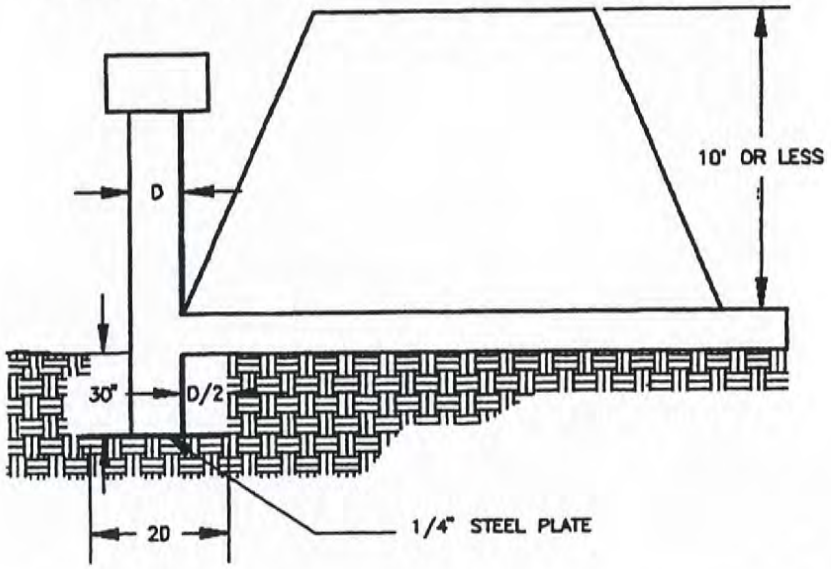
SBD = 2 x ( ) inches = ( ) inches

RISER PIPE BASE CONDITIONS FOR EMBANKMENTS LESS THAN 10' HIGH

CONCRETE BASE FOR EMBANKMENT 10' OR LESS IN HEIGHT



STEEL BASE FOR EMBANKMENT 10' OR LESS IN HEIGHT



Source: Va. DSWC

Plate 3.14-14

14. For a sediment basin, what are the bottom width, slope and minimum length of the emergency spillway requiring a flow capacity, Q = 30 cfs, given a water surface 1.0 foot above the spillway, referred to as Stage, Hp = 1.0 foot.

From ESCH III-100, Table 3.14-C:

Read the Stage, Hp (feet) in the first column, Hp = ( ) feet

Read across the table on line for Q (capacity) cfs to meet required capacity, Q = ( ) cfs

Read across the table on line for V (velocity) fps, V = ( ) fps

Read across the table on line for S (slope) %, S = ( ) %

Read across the table on line for X (channel length) feet, X = ( ) feet

Read up column to Bottom Width, b = ( ) feet

TABLE 3.14-C

DESIGN DATA FOR EARTH SPILLWAYS

STAGE (Hp) IN FEET	SPILLWAY VARIABLES	BOTTOM WIDTH (b) IN FEET																
		8	10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40
0.5	Q	6	7	8	10	11	13	14	15	17	18	20	21	22	24	25	27	28
	V	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7
	S	3.9	3.9	3.9	3.9	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8
	X	32	33	33	33	33	33	33	33	33	33	33	33	33	33	33	33	33
0.6	Q	8	10	12	14	16	18	20	22	24	26	28	30	32	34	35	37	39
	V	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0
	S	3.7	3.7	3.7	3.7	3.6	3.7	3.6	3.6	3.6	3.6	3.6	3.6	3.6	3.6	3.6	3.6	3.6
	X	36	36	36	36	36	36	37	37	37	37	37	37	37	37	37	37	37
0.7	Q	11	13	16	18	20	23	25	28	30	33	35	38	41	43	44	46	48
	V	3.2	3.2	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3
	S	3.5	3.5	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4	3.4
	X	39	40	40	40	41	41	41	41	41	41	41	41	41	41	41	41	41
0.8	Q	13	16	19	22	26	29	32	35	38	42	45	46	48	51	54	57	60
	V	3.5	3.5	3.5	3.6	3.6	3.6	3.6	3.6	3.6	3.6	3.6	3.6	3.6	3.6	3.6	3.6	3.6
	S	3.3	3.3	3.3	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2	3.2
	X	44	44	44	44	45	45	45	45	45	45	45	45	45	45	45	45	45
0.9	Q	17	20	24	28	32	35	39	43	47	51	53	57	60	64	68	71	75
	V	3.7	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8
	S	3.2	3.1	3.1	3.1	3.1	3.1	3.1	3.1	3.1	3.1	3.1	3.1	3.1	3.1	3.1	3.1	3.1
	X	47	47	48	48	48	48	48	48	48	48	49	49	49	49	49	49	49
1.0	Q	20	24	29	33	38	42	47	51	56	61	63	68	72	77	81	86	90
	V	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
	S	3.1	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0
	X	51	51	51	51	52	52	52	52	52	52	52	52	52	52	52	52	52
1.1	Q	23	28	34	39	44	49	54	60	65	70	74	79	84	89	95	100	105
	V	4.2	4.2	4.2	4.3	4.3	4.3	4.3	4.3	4.3	4.3	4.3	4.3	4.3	4.3	4.3	4.3	4.3
	S	2.9	2.9	2.9	2.9	2.9	2.9	2.9	2.9	2.9	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8
	X	55	55	55	55	55	55	55	56	56	56	56	56	56	56	56	56	56
1.2	Q	28	35	40	45	51	58	64	69	76	80	86	92	98	104	110	116	122
	V	4.4	4.4	4.4	4.4	4.4	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5
	S	2.9	2.9	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8
	X	58	58	59	59	59	59	59	59	60	60	60	60	60	60	60	60	60
1.3	Q	32	38	46	53	58	65	73	80	86	91	99	106	112	119	125	133	140
	V	4.5	4.6	4.6	4.6	4.6	4.6	4.7	4.7	4.7	4.7	4.7	4.7	4.7	4.7	4.7	4.7	4.7
	S	2.8	2.8	2.8	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7
	X	62	62	62	63	63	63	63	63	63	63	63	64	64	64	64	64	64
1.4	Q	37	44	51	59	66	74	82	90	96	103	111	119	127	134	142	150	158
	V	4.7	4.8	4.8	4.8	4.8	4.8	4.8	4.8	4.8	4.9	4.9	4.9	4.9	4.9	4.9	4.9	4.9
	S	2.8	2.7	2.7	2.7	2.7	2.7	2.7	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6
	X	65	66	66	66	66	67	67	67	67	67	67	68	68	68	68	68	69
1.5	Q	41	50	58	66	75	85	92	101	108	116	125	133	142	150	160	169	178
	V	4.8	4.9	4.9	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.1	5.1	5.1
	S	2.7	2.7	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.5	2.5	2.5
	X	69	69	70	70	71	71	71	71	71	71	71	72	72	72	72	72	72
1.6	Q	46	56	65	75	84	94	104	112	122	132	142	149	158	168	178	187	197
	V	5.0	5.1	5.1	5.1	5.1	5.2	5.2	5.2	5.2	5.2	5.2	5.2	5.2	5.2	5.2	5.2	5.2
	S	2.6	2.6	2.6	2.6	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5
	X	72	74	74	75	75	76	76	76	76	76	76	76	76	76	76	76	76
1.7	Q	52	62	72	83	94	105	115	126	135	145	156	167	175	187	196	206	217
	V	5.2	5.2	5.2	5.3	5.3	5.3	5.3	5.4	5.4	5.4	5.4	5.4	5.4	5.4	5.4	5.4	5.4
	S	2.6	2.6	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5
	X	76	78	79	80	80	80	80	80	80	80	80	80	80	80	80	80	80
1.8	Q	58	69	81	93	104	116	127	138	150	160	171	182	194	204	214	226	233
	V	5.3	5.4	5.4	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.6	5.6	5.6	5.6	5.6	5.6
	S	2.5	2.5	2.5	2.5	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4
	X	80	82	83	84	84	84	84	84	84	84	84	84	84	84	84	84	84
1.9	Q	64	76	88	102	114	127	140	152	164	175	188	201	213	225	235	248	260
	V	5.5	5.5	5.5	5.6	5.6	5.6	5.7	5.7	5.7	5.7	5.7	5.7	5.7	5.7	5.7	5.7	5.7
	S	2.5	2.5	2.5	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.4
	X	84	85	86	87	88	88	88	88	88	88	88	88	88	88	88	88	88
2.0	Q	71	83	97	111	125	138	153	164	178	193	204	218	232	245	256	269	283
	V	5.6	5.7	5.7	5.7	5.8	5.8	5.8	5.8	5.8	5.8	5.8	5.9	5.9	5.9	5.9	5.9	5.9
	S	2.5	2.4	2.4	2.4	2.4	2.4	2.4	2.4	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3
	X	88	90	91	91	91	91	92	92	92	92	92	92	92	92	92	92	92
2.1	Q	77	91	107	122	135	149	162	177	192	207	220	234	250	267	276	291	305
	V	5.7	5.8	5.9	5.9	5.9	5.9	5.9	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0
	S	2.4	2.4	2.4	2.4	2.4	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3
	X	92	93	95	95	95	95	95	95	95	96	96	96	96	96	96	96	96
2.2	Q	84	100	116	131	146	163	177	194	210	224	238	253	269	288	301	314	330
	V	5.9	5.9	6.0	6.0	6.0	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.2	6.2	6.2	6.2
	S	2.4	2.4	2.4	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3
	X	96	98	99	99	99	99	99	100	100	100	100	100	100	100	100	100	100
2.3	Q	90	108	124	140	158	175	193	208	226	243	258	275	292	306	323	341	354
	V	6.0	6.1	6.1	6.1	6.2	6.2	6.2	6.2	6.3	6.3	6.3	6.3	6.3	6.3	6.3	6.3	6.3
	S	2.4	2.4	2.3	2.3	2.3	2.3	2.3	2.3	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2
	X	100	102	102	103	103	103	104	104	104	105	105	105	105	105	105	105	105
2.4	Q	99	116	136	152	170	189	206	224	241	260	275	294	312	327	346	364	378
	V	6.1	6.2	6.2	6.3	6.3	6.3	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4
	S	2.3	2.3	2.3	2.3	2.3	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2
	X	105	105	106	107	107	108	108	108	108	109	109	109	109	109	109	109	109

Source: USDA-SCS

Hp = Stage (feet)
Q = Flow Rate (cubic feet/second)
V = Velocity (feet/second)
S = Slope (%)

X = Min. Spillway Length (feet)
b = Bottom Width (feet)

15. What is the Saturated Length, Ls(feet), of a sediment basin barrel given the depth of water at the principal spillway crest, Y = 10 feet, slope of the barrel, S = 0.08 feet/foot, (8%) and the slope of the upstream face of the embankment is 3:1, where Z feet horizontal to one foot vertical, Z = 3 feet/foot.

$$Ls = Y \times (Z + 4) \times \left(1 + \frac{S}{0.25 - S}\right)$$

Where:
Y = Depth of water at the principal spillway crest (feet)
Z = Slope of upstream face of the embankment (feet/foot)
S = Slope of the barrel (feet/foot)

Ls (Saturated Length, feet) = Y x (Z + 4) x {1 +[S/(0.25-S)]}

Ls = ( ) feet x [( ) + 4] x {1 + [( )/(0.25 – ( )]}

Ls = ( ) feet

16. Given a depth of water at the principal spillway crest, Y = 8 feet, slope of barrel, S = 10%, the slope of the upstream face of the embankment is 2.5:1, what is the Saturated Length, Ls (feet), of the barrel?

From ESCH III-105, Plate 3.14-11:

On the bottom of the chart, read on the vertical axis the depth of water at the principal spillway crest:

Y = ( ) feet

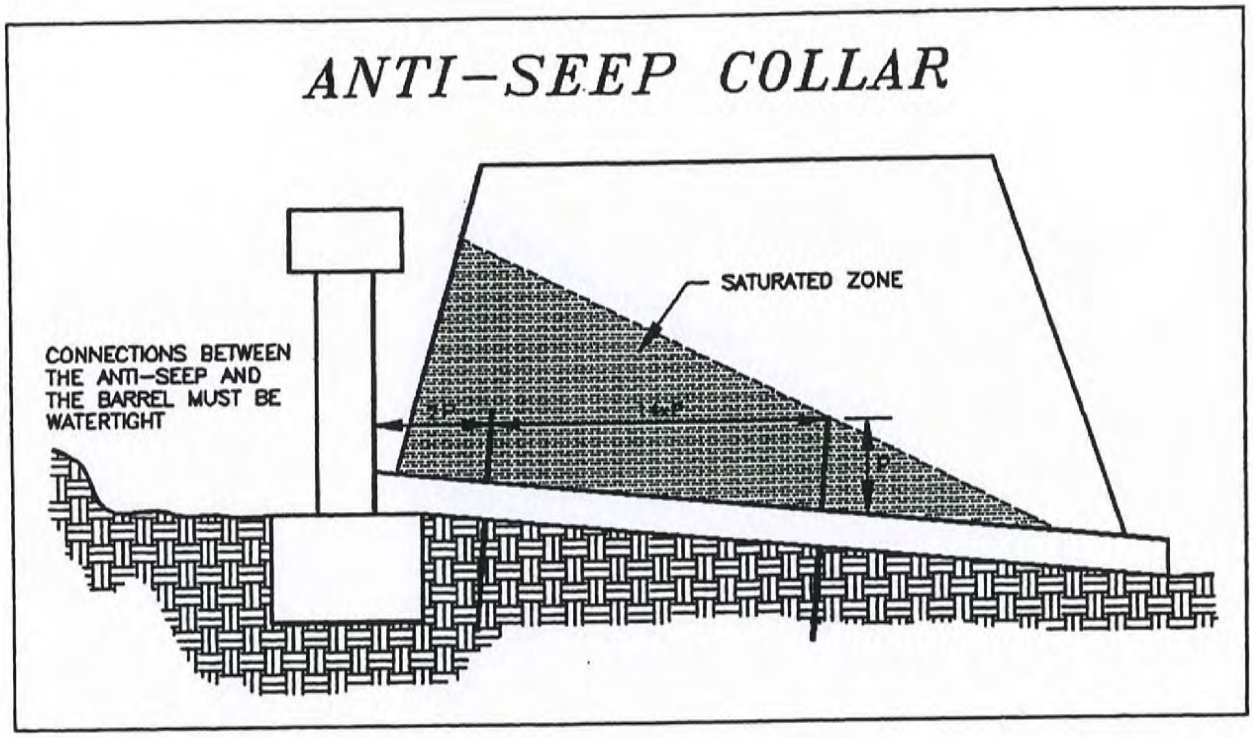
Read across chart to slope of pipe:

S = ( ) %

Read up to top of the chart to upstream embankment slope: ( ): 1

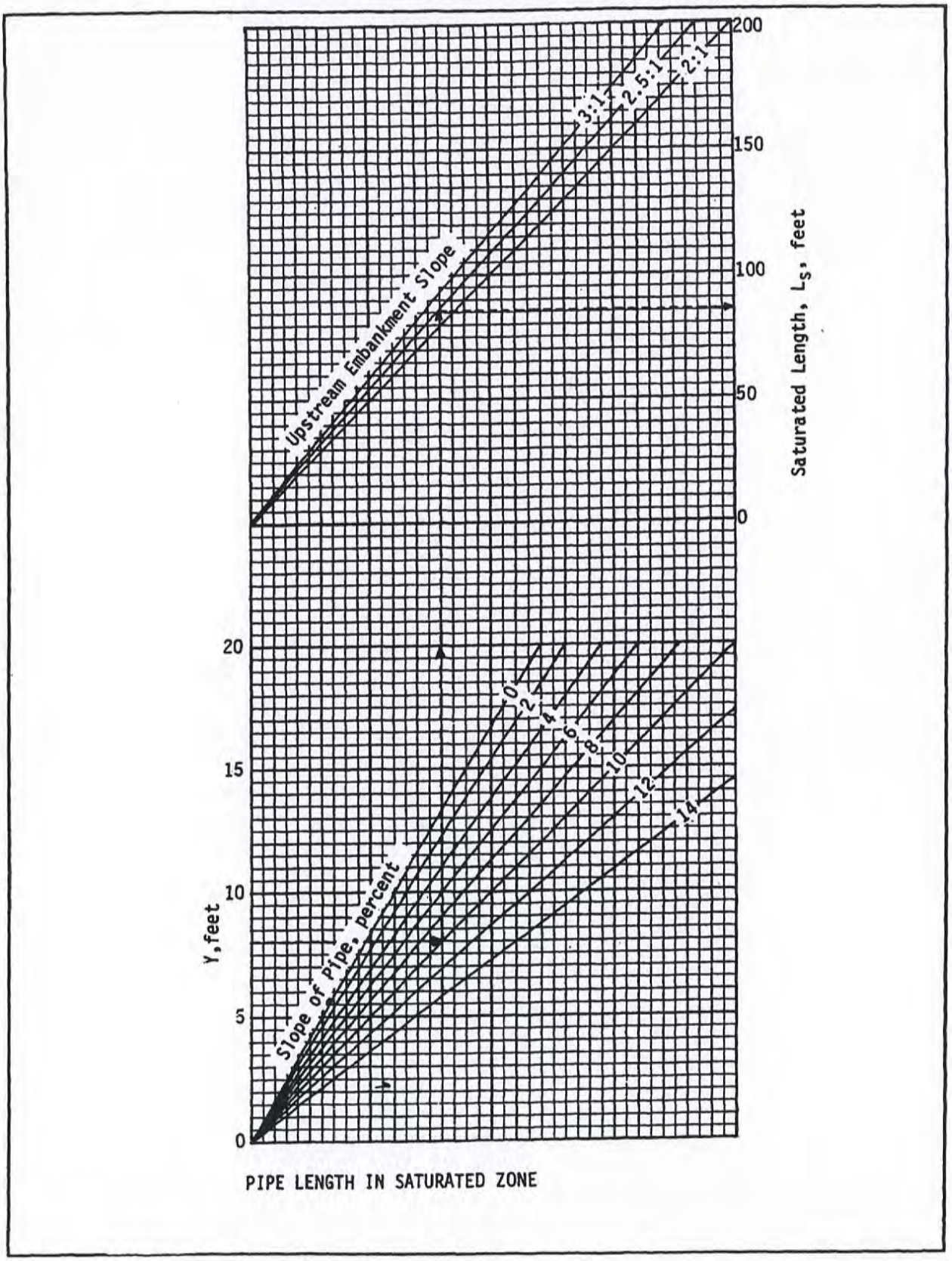
Read across chart to saturated length:

Saturated Length, Ls = ( ) feet



Source: Va. DSWC

Plate 3.14-4



Source: USDA-SCS

Plate 3.14-11

17. What is the size of two anti-seep collars given a 3 feet diameter barrel with a saturated length of 85 feet?

From ESCH III-106, Plate 3.14-12:

On the lower chart, select the saturated length.

Saturated Length, Ls = ( ) feet

Read across chart to number of collars.

Number of Collars = ( )

Read up to top of chart to pipe diameter.

Pipe Diameter, D = ( ) feet

Read across chart to size of anti-seep collars.

Size of Anti-Seep Collars = ( ) feet x ( ) feet

18. What is the maximum spacing between anti-seep collars which are 4 feet by 4 feet and attached to a 24 inch diameter barrel?

Given Collar Size, V = ( ) feet

Given Barrel Diameter, D = ( ) feet

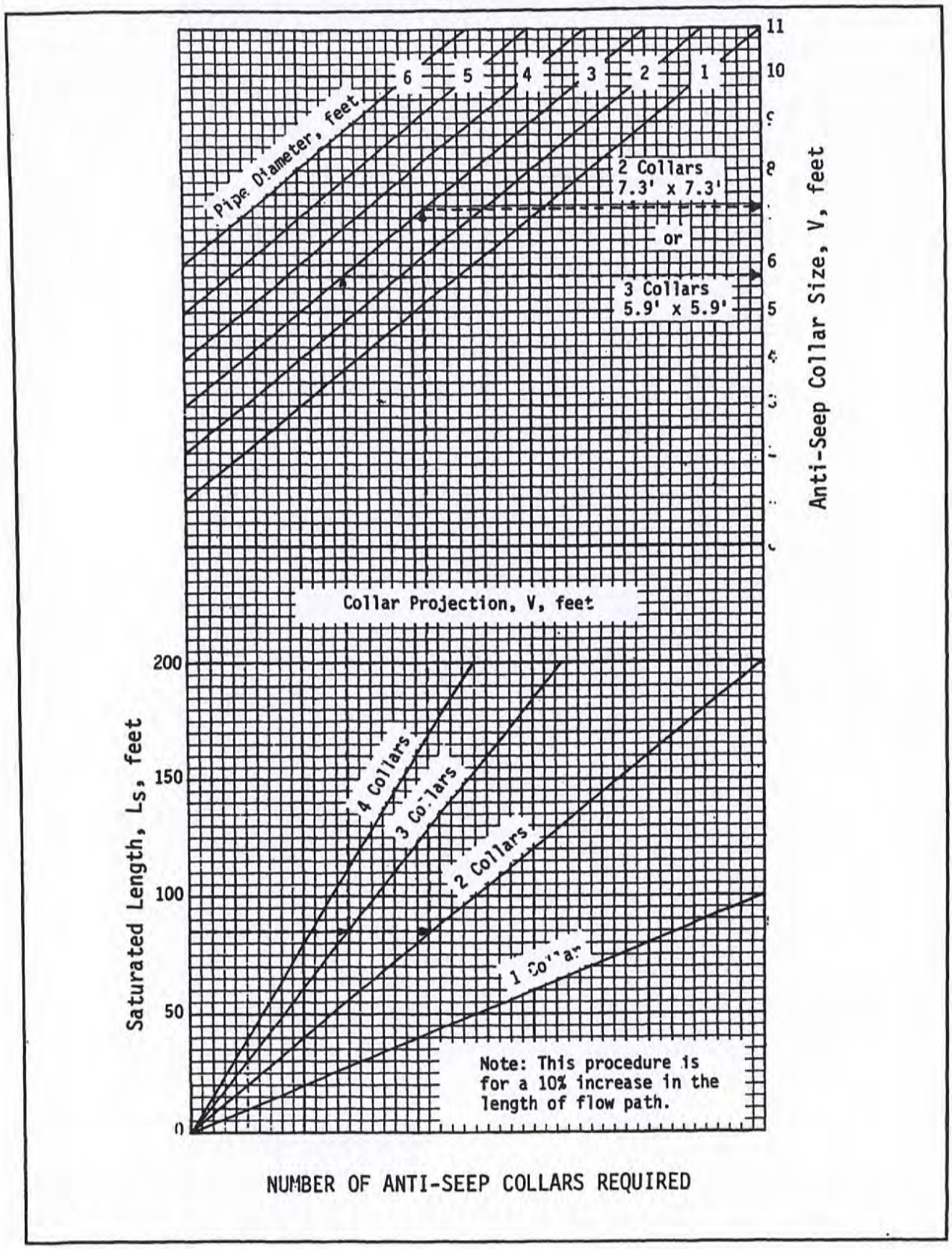
$$P = \frac{V - D}{2} \quad \textbf{and} \quad Lm = 14 \times P$$

P (Projection of Collar above barrel, feet) = (V – D) / 2

P = [( ) – ( )] /2 = ( ) feet

Lm (Maximum Spacing between Anti-Seep Collars, feet) = 14 x P (feet)

Lm = 14 x ( ) feet = ( ) feet



Source: USDA-SCS

Plate 3.14-12